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IMPROVED TELESCOPE**FIELD OF THE INVENTION**

The invention concerns the space telescopes and large membraneous mirrors.

STATE OF THE FORMER ART

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H. J. Robertson (Perking-Elmer Corporation)(A symposium on support testing of large astronomical mirrors, Tucson, Arizona, 09/12/66) describes a telescope comprising a first storey with a mirror made of a multitude of elementary mirrors, a second storey containing the focal plane, and a third storey for analysing the shape of the mirror.

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Perkins and Rohringer (US 4 093 351) describe membraneous mirrors tied to a concave surface stiffened by means of electric charges. Silverberg (WO 94/10721) describes a membraneous mirror stiffened by surface charges, and shaped by outside fields created by a rigide support.

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Le Grill (Fr 2 662 512) describes a system with a pliable membrane dependant of a rigid support which controls its shape.

Bui-Hai et Nhu (US 5 182 569) envisage, for use in ultra-high frequency, a mirror obtained by curing a rotating resin.

25

Drawbacks. All these rigid devices are very heavy.

SUMMARY OF THE INVENTION

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Space telescope 1, with three storeys 4, 5, 6, fold able to allow its putting in orbit, comprising a membraneous mirror 45, a actuating membrane 46 for shaping mirror 45, a cylindrical enveloppe 2, or an open textile tubular frame and protecting membranes 67 (Fig 21, 27), and light source 102 (Fig 45).

Pliable cylinders closed at one end.

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In an implementation (Fig 1), the enveloppe 2 of the telescope has a protecting jacket 3. They are made as cylinders closed at one end, made of composite material that can be cured under ultraviolet light or any other already known means.

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Tubular frames. In other implementations (Fig 21, 27), tubular frames are made of textile tubes 41, 42, 43 of a complexe annular structure.

5 It is unfolded by introduction of a gaz in the tubes, then rigidified after infolding by curing of a resin 54 situated in the annular structure of the tube, or cured by means of ultraviolet solar radiation.

10 **Parabolic membranes.** The membraneous mirror 45, the actuating membrane 46, and, in the case of a tubular frame, the protecting membranes 67, are made by spreading a liquid film 64 which hardens on the surface of a liquid 61 contained in a circular container 62 rotating around a vertical axis.

15 The mirror 45 and the actuating membrane 46 are tied together by means of their centrales flanges 46.4 or 46.9, either directly or by means of a cylinder 96 mounted on chamber 18.

Magnetic dipole. A magnetic dipole 142 parallel to the optical axis is rigidly tied to one of the chambers of the telescope or on its envelope (Fig 43).

20 If one electrode is implemented by a spiral shaped surface design, it works by electrostatic effect when no current flows, and by magnetic effect when a current is present.

Rotating the membranes. The membranes are infolded, stiffened, steered and stabilized by rotation.

25 **Monitoring the parabolic shape.** The monitoring of the shape of the membraneous mirror 45 is realised by a method of sagittal analysis, a derivative of the Foucault's method.

Self trained spot light telescope. In order to train a telescope used as a spot light, one use a Cassegrain type set-up fitted with a semi transparent parabolic secondary mirror 101, this in order

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to allow the light beam 103.2 to keep going towards a control device. With such set-up, the light beam generates an accessory point like image confounded with the image of the observed object (Fig 45, 46).

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The invention allows, through the displacement of the optical axis 76 of the mirror 45 within the solid angle 77 which is centered on the main optical axis 39 of the telescope (Fig 13), a scanning of

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this solid angle 77 without moving the telescope.

BRIEF DESCRIPTION OF THE FIGURES

Fig. 1- Cut away view of telescope 1 with envelope 2 and jacket 3.

Fig. 2- Bird's eye view of the telescope.

5 Fig. 3- Outside view of the jacket with stiffening tubes.

Fig. 4- Cut away view of the folding by telescopic invagination.

Fig. 5- Bird's eye view of the folding by telescopic invagination.

Fig. 6- Schematic view of the folding spokes like.

Fig. 7- Bird's eye view of the folding spokes like.

10 Fig. 8- Bird's eye view of the scrolling of the spokes.

Fig. 9- Bird's eye view of the folded telescope.

Fig.10- Cut away view of the folded telescope.

Fig. 11, 12- Devices for the folding in a spokes like manner.

Fig. 13- Scanning of a solide angle.

15 Fig. 14- Gimbal mounting.

Fig. 15- Ball joint mounting.

Fig. 16- View of the ring shaped Image at minimum of aberration.

Fig. 17- Image exploration by movable CCD.

Fig. 18, 19, 20- Folding of the mirror.

20 Fig. 21- Quadratic frame.

Fig. 22- Bird's eye view of two consecutive tubes 7.

Fig. 23- Cut away view along the optical axis and tube 7.

Fig. 24- Bird's eye view of the quadratic frame.

Fig. 26- View of an actuating electrode.

25 Fig. 27- Tripode frame in a plane containing optical axis and tube 7.

Fig. 28- Cut away view of a textile tube.

Fig. 29- Folding of a tube.

Fig. 30- Folding of the telescope.

30 Fig. 31, 32, 33, 34- Membrane on rotating liquid.

Fig. 35- View of surface designs.

Fig. 36, 37- Ring and handle for handling of the membrane.

Fig. 38- Membrane with downward flanges.

Fig. 39- Membrane with upward flanges.

35 Fig. 40, 41- Details of a central flange.

Fig. 42- Positioning of a central flange.

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- Fig. 43- Mirror and membranes for actuating and protection.
Fig. 44- Revolving containing and shaping electrodes.
Fig. 45- Laser beam and secondary mirror.
Fig. 46- Focal point, secondary mirror and tertiary mirror.
5 Fig. 47- Mirror for centering two chambers.
Fig. 48- Search of the sagittal spot.
Fig. 49- Sagittal analyser.
Fig. 50- Details of the sagittal analysing device.
Fig. 51- Polarized stacked screens.
10 Fig. 52- Upward component.
Fig. 53- Downward component.
Fig. 54- Earth bound telescope.
Fig. 55, 56- Mirror of the earth bound telescope.

DETAILED DESCRIPTION

- 15 First embodiment: cylindrical envelope closed at one end.
The three storeys 4, 5, et 6 of telescope 1 are united by a
cylindrical envelope 2 closed at one end, to which is associated a
protecting jacket 3.
Envelope 2 and jacket 3 have (Fig. 3) longitudinal tubes 7, either
20 parallel to the optical axis 39, or helicoidal 9 that can,
according to the former art, be stiffened by a gaz pressure.
Insufflation of gaz will restore the original shapes of the
telescope envelope and of its protective jacket.
In one special implementation, the space between the jacket and
25 the telescope is closed by a ring 10.
Tubes 11 stiffen the openings which are maintained roughly
elliptical by means of centering straps 12 and 13.
Truncated or bitruncated cylindrical envelopes closed at one end.
In a particular implementation, in order to facilitate folding,
30 the cylindrical envelopes closed at one end are slightly truncated
or bitruncated.
Vertical telescope folding. In a particular implementation of the
invention, the large diameter, centered, cylinder 14 (Fig 4) is
manufactured before folding either entirely or of such sufficient
35 length as to allow partial folding.

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Bottom 15 is added after the first stage of folding.

Whenever the telescope envelope 2 is concerned, the three storeys 4, 5, et 6 are tied to the jacket by their arms before folding, or during the folding (Fig. 4 and 5).

5 Folding by telescopic invagination. A cylindrical element 16 of cylinder placed in a vertical position is used as starting element.

10 This cylindrical element is maintained by external means and the part of the cylinder which is above this element is introduced inside the cylinder by folding along a circle, then push downwards until such determined height as seen fit.

In this situation, one secures the first vertical fold so obtained just above the starting cylindrical element, or slightly under, and one resumes with a new folding procedure.

15 In this manner, the total part of the cylinder above the starting cylindrical element 16 finds itself folded within the height of this starting cylindrical element 16, or slightly greater height, this in order to create, with the starting element a cylindrical torus with a thickness roughly equal to the sum of the thickness
20 of all the different folds.

The same procedure takes place with the bottom part of bitruncated cylinder of the telescope envelope.

One therefore has a stack of all three telescope storeys and elementary folding 17 of the bevelled sun shade.

25 The mirror storey chamber 18 is stretched downwards by a centered mast 21 allowing communications between the telescope and the outside, this mast carrying solar panels, reactive means of positioning and telecommunication means, not shown.

30 Folding telescope in a spokes like manner. According the former art, each stage of the telescope is made of a central chamber tied, by three or four arms 23 (Fig. 2 and 4) to a cylinder 2 closed at one end

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The vertical folding by invagination having been achieved, the three chambers are stacked. The nine or twelve arms are stacked as well, three by three.

Folding telescope in a spokes like manner, according to the

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Invention, is then implemented with a number of spokes multiple of 3 or 4.

Folding telescope in a spokes like manner devices (Fig. 6 to 12).

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The folding device is made of linear vertical means 24 situated inside the cylindrical folding, some of them in contact with the ends of the arms, and holding the cylindrical folding, and vertical linear means 25 situated outside the cylindrical folding, working in pairs, and taking between two elements 25a and 25b of a pair, the spoke fold held by the internal means 24 (Fig. 7).

10

In case the internal vertical means 24 of folding be situated under the bottom of cylinder closed at one end, this bottom has holes obturable to allow the internal vertical means of folding to be removed.

15

If one displaces radially the external means 25 towards the chamber, thanks to the guides 26 and 27 (Fig. 11 and 12), the external means having a major effect and the internal means a radial elastic retaining effect, the initial cylindrical vertical folding shall take the shape (Fig. 7) of a wheel with spokes 29 in contact with central chambers.

20

Under the conjugated effect of vertical external means 25 bringing the cylindrical folding against the chambers, and the internal means 24 holding them, the part of the vertical folding situated between the spokes is pushed against the chambers.

25

The chambers arms being longer than the spokes of the folding, the arms will be folded zigzag wise during the movements of the internal and external folding means.

Scrolling of the spokes. (Fig. 8, 9, 10) According to the invention, to scroll the spokes 29 around the chambers, one create, around the central axis of the chambers, a revolving relative motion of the internal mean 24 which remain stationery

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relative motion of the internal means 21. Then, the internal means 21 are moved and push the vertical folding against the chambers. In this manner the spokes are wound around the chambers.

Then, the vertical means of folding are removed.

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Folding the jacket. The folding of jacket 3 is made easier since it is empty.

The scroll made by the telescope is placed in the center of the

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- folding device and the spoke like folding of the jacket and its scrolling is done at the contact surface, around the telescope scroll.

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The bottom of the jacket has a hole allowing the external mast 21 to go through it.

10

Crumpled folding of the bottom (Fig. 10). During the spokes folding, the bottom of the cylinder closed at one end remains always in the inside of a perimeter determined by the spoke folds. Under these conditions, the bottom 15 of the envelope 2, or 22 of the jacket, take a natural or assisted folding which is difficult to draw, and which is contained within a restricted space showed by waves 31 (Fig. 10).

15

Unfolding vertical telescope tubes (Fig. 4, 5). Unfolding vertical tubes 32 and 33 are closed tubes set up symmetrically around the close at one end cylinders 2 and 3, along a generating line.

20

They are made integral with cylinders closed at one end 2 and 3 at heights identical to those of the cylindrical elements of the telescopic folding, thanks to braces 34 and 35 (Fig 4, 5).

They are folded by telescopic vertical invagination, in the same way as the cylinders 2 and 3, in cylindrical elements of same height as that of the cylinder closed at one end and at the same time.

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Insufflating in these infolding tubes, through openings 36 and 37, of a pressurized gaz, causes their expansion and that of the cylinders 2 and 3.

They are part of the final stiffness of the cylinders 2 and 3.

Folding means. In one example of implementation (Fig. 11, 12), the internal 24 and external 25 folding means are made of movable trolleys 26 and 27 guided radially in an horizontal plane, by guides 38, and fitted with linear devices 24 and 25 perpendicular to this plane and able to take a lower or higher position.

In one particular implementation, the vertical elements are made of two or more vertical sub elements capable of relative closing motion while staying parallel to each other.

In this manner, the motion devices can grad between their vertical components the concentric fold created by the vertical folding.

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Second implementation: tubular frame. The telescope 1 (Fig. 21), with optical axis 39, has three storeys 4, 5, and 6, and has a frame 40 made of many main tubes 41, parallel and having the same length, each being divided into two portions linked to storeys 4, 5, and 6 of the telescope by parallel spacing tubes 42.

Storeys 5 is at about equal distance from storeys 4 and 6.

To these first tubes are added (Fig. 22) reinforcing tubes 43 linking elements of flexible junctions 44 of former tubes in the planes defined by the main tubes 41 taken two at a time.

Elements of junction 44 allow the continuity of the internal space of the tubes.

Mirror 45 and actuating membrane 46 are shown in a cut away including the optical axis and a tube 41, but limited to the optical axis (Fig. 24).

Active elements of the telescope are united in chambers 18, 19, and 20 located in the center of the three storeys 4, 5, and 6, and held at those centers by tubular arms, set in a star 23, and tied to tubes 41 (Fig. 24).

These arms (Fig. 25) are made of at least two tubes 23.1 and 23.2 located in the planes containing the optical axis and one tube 41, tube 23.1 being above tube 23.2.

These tubes 23.1 and 23.2 are united at one of their ends to joints 44 located at ends of tubes 41, and at their other ends to devices 23.3, as per former art, of variable length, located on or inside the chamber 18, 19, and 20 and allowing, if necessary, chambers 18, 19, and 20 to be adjusted onto the optical axis 39 of the telescope.

Electrodes or coils 23.4 are drawn on tubes 23.1 or 23.2 (Fig. 26) so as to adjust the perpendicularity between optical axis and actuating membrane, and therefore, between optical axis and mirror.

In this implementation, the mirror and its actuating and protecting membranes are inside the frame.

In a particular implementation (Fig. 27), frame tubes 41 are not parallel any more but generate a tripod pyram mast. The triangular base of the tripod mast is contained within a

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brought one or several products that immediately harden to create membrane 46.

5 Reflecting layer. A reflecting medium is put on the membrane while it is still on the rotating liquid 61, namely by the stacking layers having appropriate dielectric indices and appropriate thicknesses.

10 Surface designs. While it is still on liquid 61, the membrane 46 is locally covered, by means in accordance with the former art, with a conducting covering in the shape of the surface designs 46.1, in so doing creating a number of annular electrodes centered on the optical axis, acting upon the radius of curvature, and a number of local electrodes 46.2 acting upon local defects (Fig 35).

15 Electronic spread in the membrane. The membrane 46, while still on liquid 61, is locally covered, by means of the former art, with a thin structure identical to that of an integrated multilayer circuit having conducting, insulating or semi conducting elements, contiguous or superimposed.

20 Electrical supply of these surfaces designs is provided by surface conductors 46.2 linked to a power supply through the center of the membrane.

25 These surface designs IC, when integrated to the actuating membrane of the mirror, allows, according to the invention, through the use of a capacitive coupling between the membrane and the mirror, a self control of the distance between mirror and membrane, and consequently the stabilization of the shape of the membranes without the intervention of the central system.

30 Protecting membrane (Fig. 27, 43). According to the invention, in the case of a tubular frame, one or several parabolic membranes 67 and 67.1, having flanges 67.2 raised above mirror 45, are located behind actuating membrane 46.

According to the invention, these membranes are made of a fibrous structure impregnated with resin, the fiber being preferentially oriented parallel to the surface of the membrane.

35 Membranes 68 and 69, located at the focal point and at the sagittal analyser, protect these points from direct star light.

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A very narrow band filter 70 (Fig. 50) protects equally the monochromatic sagittal analyser from stray light.

Actuating coils. Envelope 2 of telescope 1 is fitted at its bottom, at the level of the mirror, with a coil 71 made of conducting elements 72 encircling said envelope 2 (Fig. 1). The coil so created generates, when activated by an electric current, a magnetic field parallel to the axis of the telescope. The discrete coil 73 of the actuating membrane will interact with this magnetic field, so as to maintain the desired shape of said membrane and to keep it centered on the optical axis of the telescope.

In a particular implementation, the membrane fitted with discrete coils is metallized and constitutes the mirror of the telescope.

The membrane 46 fitted with coils 73 has only an approximate shape, and the final shape is given to the mirror membrane 45, its shape being determined by the electrostatic forces existing between the conducting surface 74 of the mirror membrane and electrodes 75 present on membrane 46 which has an approximate shape and is used as actuating membrane.

Mirror control. Surface electronic circuits integrated to the membrane during manufacturing, control the potentials of the electrodes acting upon the mirror, as well as the magnetic field of the membrane coils and the magnetic field of the telescope. The metallised surface 74 of the mirror 45, or any conducting surface, should the reflective surface be dielectric, will initially be at 0 potential.

Electrodes 75 of actuating membrane 4b are set at positive or negative potentials, and as a result, decrease or increase the relative distance between mirror and actuating membrane.

30 In this manner, important local distortion of the actuating membrane 46 will not prevent getting a perfect shape for the mirror.

Surface IC receive their instructions from control electronics which themselves get their information from the sagittal analysing
35 device.

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separates long range action acting on the actuating membrane through magnetic fields interacting with the field of the coil, and short range action acting through electric field between membranes.

- 5 Field scanning (Fig. 13). This dual system allows an important movement of the mirror 45 so that the optical axis 76 of the mirror will be able to scan a solid angle 77, while keeping the quality of the image at the focal plane 78 of the telescope. This solide angle 77 is determined by the limits of the passible magnetic and electrostatic actions, in conjunction with the
- 10 mechanical characteristics of the membranes, of the energy available and of the values of the voltage of the power supplies. Mobile sagittal analyser (Fig. 13). The sagittal analyser, or any mirror control device located at the level of the sagittal
- 15 segment, moves, according to the invention, within a circle centered on the optical axis 39 of the telescope, while staying pointed toward the intersection of the ideal extended surface of the mirror 45 and said initial optical axis 39. When in a new position, away from the initial optical axis, the
- 20 sagittal analyser 79 sends to the mirror electronic control device the informations necessary to give to the mirror membrane its parabolic shape, or any other shape required for a minimum of aberrations, having their sagittal segment determined by the position of said sagittal analyser 79.
- 25 This mirror 45 will generate on the photoelectric reception matrice 80 the image 81 of objects located in a direction deviating from previous optical axis 39 at double the angle of the deviation of the optical axis of the mirror 45 as materialized by the sagittal analyser 79.
- 30 In order to compensate for loss of quality of the image 48 when far for the optical axis, the shape of the mirror 45 is optimized by the sagittal analyser 79 itself, associated or not to a control device located in the focal plane 78.
- 35 Gimbal mounting (Fig. 14). In order to point the mirror 45, the cylinder 82 is gimbal mounted along diameter 84 and 85 and actuators 86 point the axis of the cylinder towards the sagittal

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analyser.

In another implementation (Fig. 15), the mirror and membrane centering cylinder 49 is centered on ball joint 87.

5 Annular scanning (Fig. 16). In one particular implementation, the sagittal analyser remains centered on the principal optical axis 39 of the telescope.

The mirror generating line is progressively modified while preserving the mirror circular symmetry.

10 This distortion is such that the image 81 has a minimal aberration centered ring 88 which increase radially on the receiving photoelectric matrice 80, like a circular wave, in conjunction with changes of the mirror.

15 This receiving matrice 80 is scanned synchronously with the scanning of ring 88, the latest being the image with the minimum of aberration.

In this manner, the field of least aberration image can be greatly expanded.

20 In one particular implementation, one or several photoelectric receiving matrice 89 are moved in a circular or helicoidal fashion and scan the least aberration ring 88, thereby allowing scanning of a large area with photoelectric matrices of small area.

Mirror and membrane folding (Fig. 18, 19). The mirror and the actuating membrane 46 are made totally or in part of a material with shape memory.

25 After manufacturing, the mirror 45 and the membrane 46 are distorted in such a way that this distortion is retained until new conditions appear, that brings back the initial shape.

30 The membranes are concave; if one pushes (Fig. 18) the bottom of the concavity, at its center and perpendicularly to the tangent plane, it results a symmetrical circular distortion which will intrude into the concavity.

Examination of this previously concave surface then reveals a concave peripheral ring and a central convex surface.

35 This central convex surface is equally pushed in the same conditions as before, and a new element of concave centered surface can be seen.

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Pursuing with the creation of alternately concave and convex surfaces, one obtains a surface resembling a series of circular, centered waves (Fig. 18, 19, and 20).

5 The thickness of this folding can be small as one wishes. It only requires an increase in the number of waves.

Once these waves fixed according to proper physical conditions, the almost flat object so obtained can be first scrolled lengthwise and then rolled in a circle.

10 Windings for rotating field. In order to allow, in conjunction with the annular motor ring 83, the rotation of the mirror, several windings are located on the envelope 2, at the level of the mirror storey.

Powering these windings with the correct phases induces a rotating field that rotates the mirror.

15 Rotating container.

First preferred implementation (Fig. 36 and 37). The edge 63 of a circular rotating container 62 is surmounted and in contact with a ring 90 having handling means 40, such as handles allowing this ring to be grabbed and taken away from the edge.

20 The membrane 46 created when the film 64 solidifies, will stick the ring 90 thereby allowing this handling.

Second preferred implementation (Fig. 38). The outside wall 92 of the container is a surface of revolution.

25 The membrane 46 extends, by means of former art, with equal or greater thickness, on the outside wall of the container, previously coated with a non sticking product, and in so doing creating a peripheral flange 4.3 that increases the stiffness of this periphery, thereby allowing it to recover better and faster its original shape.

30 It ends with a thicker band allowing handling.

In a variation (Fig. 39), the membrane extends on the inside wall of the container in the shape of a flange 46 a higher than the

of the container in the shape of a flange 46.8 higher than the rotating liquid.
Third preferred implementation (Fig. 39, 40). Container 62 has a central circular hole 93 limited by a wall 94 holding the liquid.

The external surface of wall 94 (facing the axis) has the shape of a cylindrical or conical surface of revolution.

The membrane 46 is extended, with increased thickness, on the external surface, in so doing creating an annular central flange 46.4.

Should the membrane be an actuating membrane, these vertical bands 46.7 will be conducting and will connect at one end with the surface designs 46.1 of the actuating membrane, and at the other end with the electronic central control device by means of cylinder 96.

Fourth preferred implementation. In a variation, the membrane is extended, by a flange 46.9, in the inside surface of the wall of the container and therefore raised above the rotating liquid.

In another variation (Fig 41), the membrane extended on the inside surface of the wall of the container, goes down, along this wall, in the central opening, creating a double flange 46.10.

Two examples of layout (Fig. 43) show parallel membranes and opposite membranes.

Rotating container (Fig. 44). The generating line of the bottom 97 of the circular container 62 containing the liquid under rotation should preferably be parabolic.

Willful distorsion of the rotating liquid. In order to obtain an exact parabolic shape for the working membrane, or any other shapes close to it, one must correct the shape of the rotating liquid in view of the various possible distorsions.

According to the invention, this compensation is achieved by electrostatic forces acting upon the surface of the rotating liquid.

This electrostatic forces are actuating either between conducting liquid 61 surface and electrodes 99 and 99.1 situated above the liquid. either between the liquid surface rendered conducting by

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An automatic control of the charges brought to the electrode can be achieved by optical means at the sagittal segment.

The effect of these electrodes will be reinforced by the dielectric constant of the bottom of the container which contains ferroelectric products.

Willful distortion of the membrane 46. The shape correction is achieved after manufacturing of the membrane.

A conducting thermosensitive membrane 46 is laid on rotating liquid 61, after application of a corrective field, and elevation of the temperature, so as to have a small change of shape.

It will take the corrected shape and keep it after cooling.

Self pointed spot light telescope (Fig 45, 46). A secondary parabolic mirror 101, semi transparent according to the invention, is set in a Cassegrain type mounting.

A laser 102 located at the top of the main mirror, or recessed, sends a beam 103 having the same diameter as the secondary mirror 101.

Part of this beam 103 will be reflected towards and will constitute the beam emitted by the telescope.

The transmitted portion 103.2 will be reflected, after crossing the dioptric device 104 (onto which is the secondary mirror), by a third parabolic mirror 106 which will generate a point like image 103.3 on the back of the image receiving matrix 80.

Should this matrix be sufficiently transparent, it will be sensitized by this point like image; and if not, a second matrix 105 will be installed on its back.

Secondary mirror (Fig 46). A portion of the light rays 107 issued by the object 108 under scrutiny, after having be reflected by the main mirror 45, cross the secondary semi transparent mirror 101 and the parallel surface 110 of the diopter 104 which carries mirror 101.

In a such way, the convergent beam which forms the image 81 of the object under scrutiny will occur at the focal plane, on the receiving matrix, without any appreciable defect.

This matrix 80, or matrices 80 and 105 see at the same time the point representing the laser beam and the image of the object

under scrutiny.

A servo control of the direction of the telescope then allows the image of the object under scrutiny and the laser reference point to coincide, and therefore allows the beam to be directed towards the object.

Centering of the laser beam. If the axis of the initial laser beam 103 is not parallel to the axis of the third mirror 106, its point like image 103.3 given by the third mirror 106 is shifted away from its theoretical point on the matrix; a servo-control of former art will bring it back there.

Centering of the optical axis.

Materialising of the optical axis. Chambers 19 and 20 or chambers 18 and 19, or even elements of these chambers are made parallel by interferential means according the former art, while maintaining their spacing constant.

First preferred implementation (Fig 47). A spherical mirror 112, possibly annular, is made part of chamber 19 or 20. This mirror 112 is, according to the invention, tied to the back of third mirror 106 or, better, is an integral part of it.

The optical axis of this mirror defines, a priori, the optical axis 39 of the telescope.

The curvature center 112.1 of this mirror is located at the level of the other chamber.

If a light source 113 is placed close to the center of curvature of this mirror, the later will generate an image 114 without aberration.

If the light source is on the optical axis of mirror 112, the image is also on that axis.

According to the invention (Fig 47), the light source 113 situated on the optical axis, is the image given by a flat mirror semi-transparent 115, of a real point like source 116, which is preferably monochromatic.

This point like source 116 is a thin annular hole, made in a opaque screen, strongly lighted .

The image 114 is made of a central spot surrounded by diffracting rings.

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According to the invention, an image detection device 117 with extended capacity in grey levels, is located at the level of image 114 and perpendicularly to the optical axis.

5 According to another implementation, it can equally will be constituted of two or three strips symmetrically centered on the optical axis.

If, as a result of a relative movement of the two chambers, the image 114 of the source 113 is not anymore centered on the optical axis of the mirror, the matrix 117 will monitor a new centering.

10 To that effect, the matrix analyse the image 114 and finds the center of the central spot and of the diffraction rings.

It then puts the center on the optical axis, according means of the former art.

15 Second preferred implementation. Two or three devices of the first implementation, set symmetrically around the optical axis, clear the region of this optical axis.

This set-up is used to interlock chamber 18 and 19, or elements of these chambers.

20 Lighting a target outside of the optical axis. In order to light a target outside the optical axis, it is enough to make the spot beam, going out of the main mirror, parallel to the incoming beam. This is obtain by a modification of the laser beam 103.

Then, the point like image 103.3 of beam 103.2 on matrix 105 or on semi-transparent matrix 80 at the focal plane, is off center.

25 To bring the beam on the target, it is therefore enough to put the point like image 103.3 on a symmetrical point of the image 81 of the target 108.

Stray lights. Should the observed object not be very bright, it will be located classically by two or three stars.

30 In this fashion, if the light diffused by the laser beam while crossing the various media is enough to blot out the targeted object, these stars, being much more luminous, will insure the correct pointing.

Interferential filter.

According to the invention (Fig

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shape of a portion of a sphere, protect the front end of the image receiving matrix 105 from the monochromatic laser beam 103.

5 **Second preferred implementation.** An interferential filter, possibly having the shape of a portion of a sphere, protects the receiving matrix from stray light emanating from the sagittal analyser.

10 Choosing a monochromatic sagittal analyser source having the same wave length as the laser, will enable the same interferential filter to protect the matrix from stray light coming from the laser.

Third preferred implementation. Inserting an interferential filter transmitting only the received wave length, allows to do away with filtering the stray light coming from the sagittal analyser.

15 **Mask mirror.** The center of the semi-reflecting mirror 101 is totally reflecting on the same surface as matrix 105.

In this manner the laser beam 103 will not reach the image receiving matrix 80.

20 **Sagittal analyser.** For each particular curve of revolution there exists a biunivocal relation between a point 120, or 120.1 of the sagittal segment 119 and the radius 121, or 121.1 of a centered ring of the surface of revolution.

If one knows the relation supposed to exist between the radius 121

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shape of a portion of a sphere, protect the front end of the image receiving matrix 105 from the monochromatic laser beam 103.

Second preferred implementation. An interferential filter, possibly having the shape of a portion of a sphere, protects the receiving matrix from stray light emanating from the sagittal analyser.

Choosing a monochromatic sagittal analyser source having the same wave length as the laser, will enable the same interferential filter to protect the matrix from stray light coming from the laser.

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Mask mirror. The center of the semi-reflecting mirror 101 is totally reflecting on the same surface as matrix 105.

In this manner the laser beam 103 will not reach the image receiving matrix 80.

Sagittal analyser. For each particular curve of revolution there exists a biunivocal relation between a point 120, or 120.1 of the sagittal segment 119 and the radius 121, or 121.1 of a centered ring of the surface of revolution.

If one knows the relation supposed to exist between the radius 121 and point 120, one can modify the surface under investigation in order that it satisfies this relation (Fig 49, 50).

Light source of sagittal analyser. To avoid a defect of revolution of the mirror, the light source 122 must be on the optical axis 39 of the mirror (Fig 47).

It cannot be physically on this axis since this axis is on the sagittal segment that must be examined.

According to the invention, a semi-transparent mirror 123 generates the virtual image 124 of the source 122 on the optical axis, a location chosen to be the bottom of the sagittal segment 119.

In this manner, this light source can be more easily be complex.

It will be, according to the invention, the point like image of a monochromatic laser beam 125 as generated by the semi-transparent

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mirror 123.

Acquisition of the image (Fig 48). As soon as the mirror 45 is stiffened by electrostatic charges and by rotation, it generates a blob-image 126 of source 124 of the sagittal analyser, image centered on its optical axis 39.1.

This image can be very far from the teoretical axis 39 of the telescope, and consequently very far from the sagittal analyser.

Auxiliary screen. According to the invention, a large size auxiliary screen 127, perpendicular to the optical axis 39 is situated beyond the sagittal analyser (Fig 48), or on this side but in that case with a central aperture having the side of the sagittal analyser. The non pinpoint image 126 of the sagittal analyser source 124 appears on screen 127.

An electronic camera examines this screen and take hold image 126 of source 124.

The electronic control device of the mirror 45 brings this image at the center of screen 127 where the sagittal analyser stands.

This sagittal analyser centers image 126 on its own center, located on the desired optical axis 39.

Control principle. This sagittal analyser is made (Fig 50), according to the invention, of a photoelectric matrix 128 and a screen 129 scanning the sagittal segment 119 of the mirror 45. This opaque screen 129, perpendicular to the optical axis 39, and with hole 131 centered on this axis at a particular point 120 of the sagittal segment 119, intercepts the conical sheets that do not pass through point 120 and does not intercept the conical sheet which passes through this point of the sagittal segment.

This conical sheet leans upon a ring of radius 121 of mirror 45, and trace a ring of radius 130 on the photoelectric matrix 128.

The radius 130 of this ring is proportional to the corresponding radius 121 of the mirror 45 being scrutinized.

When hole 131 explores the sagittal segment 119, the ring of radius 130 goes over photoelectric matrix 128.

One can establish a particular correspondance between points 120 of the sagittal segment and the radius of the corresponding rings. Sagittal segment examining matrix.

First preferred implementation. According to the invention, the photoelectric matrix 128, with extended capacity in levels of grey, perpendicular to optical axis 39 and centered on this axis, is located at some distance from the sagittal segment 119, going away from the mirror.

According to the invention, the photoelectric matrix is a portion of sphere centered on the middle of the sagittal segment.

Second preferred implementation. According to the invention, the matrix can be reduced to a number of matricial segments centered on the optical axis and equally distributed around this axis.

Sagittal analyser screen.

First preferred implementation (Fig 50). The screen 129 is, according to the invention, a photoelectric matrix whose central pixel is replaced by a hole 131.

This matrix 129 is capable of a movement parallel to the optical axis 39, in so doing enabling hole 131 to explore the desired sagittal segment 119.

The advantage of a photoelectric matrix over the screen stands in the fact that the matrix can center the spot image 126 on the active area, from the start of control of mirror 45, and can re center again after any operating incident.

Second preferred implementation (Fig 51). The mobile screen 129 is replaced by a stack of polarizing cells 129.1, particularly liquid crystals, having an inactive central portion 131.1.

These cells can simulate a flat screen having a hole 131 on the optical axis 39 and moving perpendicularly to its plane.

In a particular implementation, the polarizer is unique and the polarizing screens are made of crossed analysers.

Third preferred implementation. The central portion of mirror 45 is not used.

The mirror examining matrix 128 has a central aperture through which pass a cylinder 132 at the end of which is a photoelectric matrix 133 centered on the optical axis 39.

The cylinder can move along the optical axis and can therefore explore the sagittal segment 119.

When the spot image 126 is brought on matrix 128, this latest

This image can be very far from the teoretic axis 39 of the telescope, and consequently very far from the sagittal analyser.

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An electronic camera examines this screen and take hold image 126 of source 124.

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Control principle. This sagittal analyser is made (Fig 50), according to the invention, of a photoelectric matrix 128 and a screen 129 scanning the sagittal segment 119 of the mirror 45. This opaque screen 129, perpendicular to the optical axis 39, and with hole 131 centered on this axis at a particular point 120 of the sagittal segment 119, intercepts the conical sheets that do not pass through point 120 and does not intercept the conical sheet which passes through this point of the sagittal segment.

This conical sheet leans upon a ring of radius 121 of mirror 45, and trace a ring of radius 130 on the photoelectric matrix 128.

The radius 130 of this ring is proportional to the corresponding radius 121 of the mirror 45 being scrutinized.

When hole 131 explores the sagittal segment 119, the ring of radius 130 goes over photoelectric matrix 128.

One can establish a particular correspondance between points 120 of the sagittal segment and the radius of the corresponding rings. **Sagittal segment examining matrix.**

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astronomical telescope.

It also has a flange 45.4 intruding into the central hole 139 of the rigid circular support 138.

These flanges allow the periphery and the central portion of the mirror to be centered, and also allow its central electrical connection.

Rigid circular support.

First preferred implementation. The rigid circular support is fitted with surface electrodes 46.1 which allow control of the shape of the mirror under the control of the sagittal analyser of chamber 20.

According to the invention, this rigid circular support supports a parabolic membrane 46 slightly stretched by a small under pressure, in such a manner as not to alter its initial parabolic shape.

Active annular cover 140 and 141, fitted with surface devices facing the mirror 45, help in controlling the edge and the central portion of this mirror.

Space telescope with detachable mirror storey (Fig 52, 53). In such particular embodiment, the telescope 1 is made of two separated elements reunited in space after installation of the mirror and the actuating membrane in mirror storey 4.

Envelope 2 and jacket 3 are each made of two separate elements which can be associated:

- a) the upper cylindrical open element comprising focal plane storey 5 and storey 6 containing the centre of curvature,
- b) the lower cylindrical closed element comprising mirror storey 4.

A linking device allows the reunion of these two elements.

Integrated inflatable circular tubes 8, and envelope-jacket linking rings 10 maintain the circular shape of the bottom of the upper element and the top of the lower element.